Hexagonal convection patterns in atomistically simulated fluids

D. C. Rapaport
Physics Department, Bar-Ilan University, Ramat-Gan 52900, Israel
(Received 7 August 2005; published 14 February 2006)

Molecular dynamics simulation has been used to model pattern formation in three-dimensional Rayleigh-Bénard convection at the discrete-particle level. Two examples are considered, one in which an almost perfect array of hexagonally shaped convection rolls appears, the other a much narrower system that forms a set of linear rolls; both pattern types are familiar from experiment. The nature of the flow within the convection cells and quantitative aspects of the development of the hexagonal planform based on automated polygon subdivision are analyzed. Despite the microscopic scale of the system, relatively large simulations with several million particles and integration time steps are involved.

DOI: 10.1103/PhysRevE.73.025301 PACS number: 47.54.—r, 02.70.Ns, 47.27.T—

The spontaneous emergence of flow patterns in externally driven fluids is one of the more fascinating aspects of fluid dynamics, and a great deal of experimental and theoretical effort has been spent studying such phenomena over the past century. Theoretical fluid dynamics has successfully ignored the underlying atomicity, describing the dynamics in terms of nonlinear partial differential equations for continuous fields; the analysis of flow instability within this framework demands approximations whose consequences are not always readily assessed. Ideally, one would like to understand flow instability in terms of the behavior at the microscopic level by looking beyond the continuum representation to address the dynamics of the molecules themselves, albeit at considerable computational cost; given that sufficiently many molecules are followed for an adequate time interval, one can reasonably expect to see the same kind of behavior (initially in a qualitatively correct form, then, with even larger systems, also quantitatively). The ability to simultaneously encompass the dynamics both at the molecular level and the scale at which the cooperativity underlying structured flow becomes manifest is an important step in trying to break free of the limitations of traditional continuum fluid dynamics.

Accomplishing this goal calls for molecular dynamics (MD) simulation, a technique in broad general use, but less so for fluid dynamics (quite likely due to Avogadro’s tyranny—an apparent need for extremely large systems to accommodate the phenomena). A very early MD effort related to bridging the gap between atomistic dynamics and fluid behavior at the continuum level was understanding long-time effects due to correlations in atomic trajectories [1], but it was only much later that actual MD simulation of complex flow was attempted. Initial efforts were confined to two dimensions, starting with the wakes of obstructed flows [2,3] and followed by Rayleigh-Bénard (RB) convection [4–9]: the study of Taylor-Couette flow [10,11] demonstrated that complex three-dimensional flow could also be dealt with and, subsequently, the Rayleigh-Taylor instability was also modeled [12]. Other instances of MD contributing to fluid dynamics include the moving interface between immiscible liquids undergoing Poiseuille flow [13] and droplet breakup in liquid jets [14]. The present study describes the application of the MD approach to the full three-dimensional RB problem, where the behavior is potentially far richer than in two dimensions, and where simulation is more closely related to experiment; the ability to tackle increasingly demanding MD simulations, both in terms of size and duration, reflects the availability of increasingly powerful and affordable computing resources.

The RB phenomenon—the rich variety of flow patterns produced by convection in a fluid layer heated from below—continues to be a problem of great interest [15–19]. The principal dimensionless quantity governing the behavior is the Rayleigh number, $\text{Ra}=\alpha g L_2^3 \Delta T/\nu \kappa$, where $\alpha$, $\nu$, and $\kappa$ are the thermal expansion coefficient, kinematic viscosity, and thermal diffusivity, $L_2$ is the layer height, $g$ the gravitational acceleration, and $\Delta T=T_h-T_c$ is the temperature difference between the lower hot wall $T_h$ and the upper cold wall $T_c$; a critical value $\text{Ra}_c$ marks the onset of convection, where buoyancy overcomes viscous drag, and convection replaces conduction as the preferred thermal transport mechanism.

The theory is simplified by the Boussinesq approximation, in which it is assumed that the only temperature-dependent fluid property is the density. $\text{Ra}_c$ can be computed for various kinds of boundary conditions [15], as can the wavelength $\lambda$ of the convection pattern at criticality, but not the actual planform (e.g., rolls, spirals, and hexagons). Roll width (typically $=L_2$) represents a compromise; wide rolls reduce both viscous drag and diffusive heat transfer between ascending and descending cold streams, whereas narrow rolls reduce shear losses close to nonslip walls. Hexagonal patterns were once associated with non-Boussinesq fluids [18,20] (and are better known in convection driven by surface tension); the flow direction at the cell center is determined by the temperature dependence of $\nu$ and differs for gases and liquids. Hexagons are now known to occur in (essentially) Boussinesq systems above $\text{Ra}_c$ [21,22], even forming coexisting regions with opposite flows at the cell centers, a phenomenon not attributable to variable $\nu$.

The MD simulation [23] considers a fluid of soft-sphere atoms with a short-ranged, repulsive interaction $u(r) = 4\varepsilon [\sigma/r]^{12} - [\sigma/r]^6$, with a cutoff at $r_c = 2^{1/6}\sigma$. In the di-

*Electronic address: rapaport@mail.biu.ac.il
mensionless MD units used subsequently, $\sigma$ and $\epsilon$ determine length and energy, while temperature is defined by setting $k_B=1$; in the case of argon, $\sigma=3.4 \AA$, $\epsilon/k_B=120$ K, and the unit of time is 2.16 ps. The top and bottom thermal walls of the system are each formed from a layer of fixed atoms arranged as a lattice, spaced to ensure roughness and impenetrability; lateral boundaries are periodic. The temperature gradient is produced by rescaling the velocities of those atoms adjacent (within a range of 1.3) to the thermal walls; rescaling occurs every 20 time steps to allow the effect to propagate without unduly affecting the dynamics, and is applied to atoms moving away from the walls. In the initial state, atoms are placed on the sites of a regular grid, with random velocities corresponding to a uniform vertical temperature gradient. The integration time step is 0.004. In view of the extensive computations required, parallel processing based on spatial decomposition is used.

Flow analysis entails spatial coarse graining, in which a grid subdivision is applied to the region and the mean properties (velocity, temperature, density) for each grid cell are evaluated for its occupant atoms. This is repeated every 20 time steps and averages over 10 successive measurements recorded, with typical grid sizes of 5–6 horizontally and 3 vertically (≈50 atoms per grid cell); this represents a compromise between capturing the fine spatial and temporal detail of the developing convection patterns and reducing the noise due to thermal fluctuations.

Two of a series of runs are described in detail below; the eventual outcomes of both are organized convection cell patterns, a hexagonal array in the case of system A and a set of eventual outcomes of both are organized convection cell patterns, ranging from red for hot to blue for cold in the color online version. The distribution at the end of the run appears in Fig. 3, with the periodic cell array clearly visible. Superimposed on this image is a polygon subdivision produced by an automated Voronoi analysis of a slice through the flow structure (limited system size cannot accommodate the large aspect ratios $L_x/L_z>100$ used experimentally, as opposed to 15 here, that yield extended patterns amenable to Fourier and other forms of analysis [24]); cell centers marked by white spots are located at each of the local temperature minima (or at the downward flow maxima) and the plane subdivided into polygons in which the region nearer to a particular center than to any other is assigned to its polygon. The resulting polygon set provides a good fit to the cell boundaries where hot upward flow is strongest (the fit quality improves as the run progresses), and is used in the quantitative analysis below.

layer, with cold fluid descending at the cell centers. The cell array is free to orient itself to accommodate a preferred $\lambda$ for the particular size and shape of the periodic container; animated three-dimensional visualization allows following the pattern development as cells grow and merge (not shown).

Figure 2 shows the horizontal temperature distribution at a distance $=L_x/5$ from the hot wall early in the run, after the onset of convection but before a regular cell pattern develops. The distribution at the end of the run appears in Fig. 3, with the periodic cell array clearly visible. Superimposed on this image is a polygon subdivision produced by an automated Voronoi analysis of a slice through the flow structure (limited system size cannot accommodate the large aspect ratios $L_x/L_z>100$ used experimentally, as opposed to 15 here, that yield extended patterns amenable to Fourier and other forms of analysis [24]); cell centers marked by white spots are located at each of the local temperature minima (or at the downward flow maxima) and the plane subdivided into polygons in which the region nearer to a particular center than to any other is assigned to its polygon. The resulting polygon set provides a good fit to the cell boundaries where hot upward flow is strongest (the fit quality improves as the run progresses), and is used in the quantitative analysis below.

The final state of system A is shown in Fig. 1 as a streamline plot that reveals the full three-dimensional flow structure; the curved tracks (color coded to show temperature variation) are derived from the coarse-grained grid (size 96 $\times$ 82 $\times$ 12). The most prominent feature is the array of hexagonal convection cells extending across the full depth of the lower wall.
The time dependence of two prominent features of the polygon arrays is shown in Fig. 4. The polygon count falls from an initial value of \( \approx 30 \) to the eventual 8 at time \( t = 5000 \), then increases to 9 and finally drops back to 8 at \( t = 8000 \) as cells split and merge; this behavior is an indication of the slow relaxation processes that the simulations must be able to cover. The mean deviation of the polygon shape from regularity, expressed as the range of radial distances of the nearest and furthest vertices of each polygon, shows a more gradual convergence to the final value of 4.5, which is just 5% of the mean radius. Other planform properties include the mean distance from the center to the nearest point on an edge, \( \lambda_{\text{hex}}/2 \), whose final value is 93\( \pm \)1, the mean polygon area that is inversely proportional to the count, and the area variation that falls to a minimum of \( \pm 2\% \) of the mean in the final state. The average number of vertices per polygon must be 6; the spread of values falls to zero as the final state is neared. These results quantify what is observed directly, namely an initially disordered set of small convection cells that grow, merge, and rearrange, culminating in what appears to be a stable array of hexagonal cells; the final wavelength \( \lambda_{\text{hex}} = 5.27L_z \), a value not much larger than the experimental 4\( L_z \) \( \approx 20 \text{cells} \) [21] (a lower \( \lambda_{\text{hex}} \) is reported in [22]); the characteristic size of the cells present in the early, irregular pattern is about half this value (Fig. 2).

Details of the flow profile inside a single convection cell appear in Fig. 5. The arrow plot shows the radial and vertical components of the flow field within the cells, averaged over all cells of the final state, and is evaluated by projecting the flow velocity onto a series of vertical planes arranged as radial spokes around each cell center, with only grid cells that intersect the planes contributing. The maximum arrow length corresponds to a speed of 0.52. While average descending flow appears faster than ascending, this is consistent with the toroidal roll shape that allows more space for the latter. The nonslip nature of the flow at the lower wall is partly masked by coarse graining, but flow rate is seen to decrease near the wall (the effectiveness of the nonslip mechanism is better appreciated in small systems run interactively). Local temperature (not shown) increases radially outwards from the cell core and drops with height; its estimation is problematic because the contribution of nonuniform bulk flow cannot be fully removed, and thermalization includes atoms interacting with the walls, so the measured range is 0.84–11.4 (rather than 1–10), but the gradual variation across the roll profile and the absence of high gradients near the walls (except where the cool downflow initially encounters the hot wall) are evidence of efficient heat exchange between fluid and walls. Local density varies from 0.58 at the cell core to 0.38 at the periphery (the overall mean is 0.4).

The final state of run B consists of a set of six pairs of counter-rotating rolls. Figure 6 shows the streamline plot; the wavelength \( \lambda_{\text{roll}} \) (2 \( \times \) roll diameter) \( = 87 \times 2.46L_z \) (note that seven roll pairs would have produced a value close to the theoretical \( \lambda_{\text{roll}} = 2.016L_z \) [15]). The wavelength ratio from runs A and B is \( \lambda_{\text{hex}}/\lambda_{\text{roll}} = 2.14 \); the experimental ratio for coexisting hexagons and rolls is 1.2–1.3 [21]. At an early stage in run B there is an unsuccessful attempt to form a pair of longitudinal rolls.

When \( T_1 \) is lowered to 6 the roll pattern in system B is unchanged, but at \( T_1 = 4 \) the results are noisy and roll structure is not readily discerned, though it is still present in weakened form. Strong finite-size effects due to small \( L_z \) erase any hint of a sharp transition between conducting and
convecting states. The fluid has its own intrinsic thermodynamic and transport properties determined by the soft-sphere model and, since $\Delta T/T_0$ is large, does not satisfy the Boussinesq condition; estimating $Ra$ based on the Enskog theory and a simple equation of state [7,8] is inappropriate here due to the variation of $\nu$ and $\kappa$ across the layer.

These simulations (and work in progress) provide strong confirmation that MD is capable of reproducing known fluid dynamical behavior; the unique aspect of this approach is that, while following the dynamics at the atomic scale where the underlying causes of flow instability and self-organization are to be found, it simultaneously embraces the continuum scale where fluid behavior is manifest and scant evidence of atomism remains. Increasing computer performance (parallel computers are ideal for simulations of this kind) allows ever larger systems to be modeled, although this growth is tempered by the fact that computation time increases not only in proportion to system size but also due to slow diffusive processes that govern structure development. Larger systems reduce the necessarily high thermal and velocity gradients and help eliminate spurious finite-size effects, allowing closer correspondence with experiment. The outcome of the present MD study has obvious implications for future MD exploration of fluid dynamical phenomena.

This work was begun during a visit to the University of Edinburgh that was supported by the TRACS program at EPCC; S. Pawley is thanked for his kind hospitality.